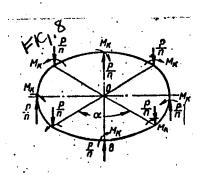
30373 S/572/61/000/007/004/006 D221/D302

Calculating flexural ...

Legend to Fig. 8: The diagram for calculating a connected ring.



Card 4/4

BIRGER, I.A., doktor tekhn.nauk, prof.

Determining the yield of intermediate parts of a threaded joint.

Vest. mash. 41 no. 5:41-44 My 161. (MIRA 14:5)

(Fastenings)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

MALININ, Nikolay Nikolayevich; BIRGER, I.A., doktor tekhn. nauk, prof., retsenzent; PONOMAREV, S.D., doktor tekhn. nauk, prof., red.; BYSTRITSKAYA, V.V., red. izd-va; UVAROVA, A.F., tekhn. red.

[Strength of turbomachines]Prochnost' turbomashin. Moskva, Mashgiz, 1962. 291 p. (MIRA 15:10) (Turbomachines)

THE PROPERTY OF THE PROPERTY O		
BIRGER	, I.A.	
*	Methods of determining residual stresses in disks. 28 no.7:859-864 162. (Strains and stresses) (Metals—Testing)	Zav.lab. (MIRA 15:6)
•		

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

S/032/62/028/005/007/009 B117/B101

AUTHOR:

Birger, I. A.

TITLE:

Methods of determining residual stresses in bars and plates

PERIODICAL:

Zavodskaya laboratoriya, v. 28, no. 5, 1962, 599-604

TEXT: Mechanical methods of determining residual stresses in samples during the removal of metal layers are discussed in detail. These methods have already been discussed by a number of other authors (N. N. Davidenkov, Ye. M. Shevandin, M. M. Saverin, M. A. Babichev, L. A. Glikman, D. I. Grekov) earlier. They consist in determining the surface tensions by measuring deformations appearing in the sample after removal of the metal layers. The deformations are assumed to be of a plastic nature. Equations for determining the residual stress in bars with rectangular or any cross section, as well as in plates are derived. The English-language reference reads as follows: R. Treuting, W. Read., J. of Appl. Phys., v. 22, no. 2, Febr. (1951).

Card 1/1

CIA-RDP86-00513R000205320015-3"

10.7100

S/032/62/028/007/009/011 B104/B102

AUTHOR:

Birger, I. A.

TITLE:

Methods of determining residual stresses in disks

PERIODICAL: Zavodskaya laboratoriya, v. 28, no. 7, 1962, 859 - 864

TEXT: Four methods are described and compared: (1) a drilling method in which the radial displacements and circular deformations are determined at the internal and external radii of the disk; (2) an 'annular' method, in which a ring is cut out of the disk, and the resulting changes in size are determined; (3) another 'annular' method whereby the changes in diameter are determined; (4) a 'cubic' method, in which strain gauges are affixed to the disk, and cubes are then cut out. Formulas are derived for calculating the residual stresses from the changes in shape of the disk as determined by the four methods. The first method requires strain gauges or a precise measuring microscope. Using either of the 'annular' methods the mutual displacements of the measuring points are greater. The 'cubic' method is very simple, but the stress pattern is difficult to obtain. There are 6 figures.

Card 1/1

APPROVED FOR RELEASE: 06/08/2000

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40670 \$/032/62/028/009/004/009 В104/В102

10.6200,

AUTHOR:

Birger, I. A.

TITLE:

Determination of the residual stresses in thin-walled tubes

PERIODICAL: Zavodskaya laboratoriya, v. 28, no. 9, 1962, 1112 - 1117

TEXT: Formulas for determining residual stresses in thin-walled tubes by the ring and strip method are derived. With the ring method the residual stress in the ring zone (da) is made up as follows: $\sigma_{Q}^{*}(a) = \sigma_{Q}(a)$ + $\sigma_{Q1}(a) + \sigma_{Q2}(a) + \sigma_{Q3}(a)$, where $\sigma_{Q}^{*}(a)$ is the circular residual stress in the zone da (Fig. 1), $\sigma_{Q}(a)$ is the original circular residual stress in the zone a and the other three terms represent the residual stresses produced by cutting off the ring, slitting it and chipping off thin layers. Using the strip method a small strip is cut out of the tube and the residual stress is determined from its deformation (Fig. 5). $\sigma_{ZN} = \sigma_{Z} + \sigma_{ZB}$ holds for the residual stress in the strip where σ_{Z} is the axial residual stress in the tube and σ_{ZB} the additional stress in the strip due to cutting out. Card 1/4

Determination of the residual...

5/032/62/028/009/004/009 B104/B102

Expressions are worked out for all of the terms and are used to give

$$\sigma_{\theta}(a) = \frac{1}{1 - \mu^{\theta}} \{ F_{\theta}(a) + \mu F_{\theta}(a) \}; \qquad (27)$$

$$\sigma_{\theta}(a) = \frac{1}{1 - \mu^{\theta}} [F_{\theta}(a) + \mu F_{\theta}(a)]. \qquad (28)$$

where

$$F_{g}(a) = 2 \frac{E \delta_{p}}{D_{cp}^{2}} \left(\frac{h}{2} - a\right) - \frac{1}{3} \frac{E(h - a)^{2}}{3} \times F_{g}(a) = -\frac{8E}{l^{3}} I_{g} \left(\frac{h}{2} - a\right) + \frac{4E}{3l^{3}} \left[(h - a)^{2} + \frac{d\delta}{da} + \frac{2E}{3} \int_{0}^{a} \frac{2h - 3a + \xi}{D^{3}(\xi)} \frac{d\delta}{d\xi} d\xi. \quad (20) \right]$$
and
$$+2 \int_{0}^{a} I(\xi) d\xi \left[. \quad (26), \quad ($$

The method by N. N. Davidenkov (Zhurnal tekhnicheskoy fiziki, v. 1, no. 1 (1931)) is improved by taking account of the stresses that occur in cutting out the strips, obtaining:

Card 2/4

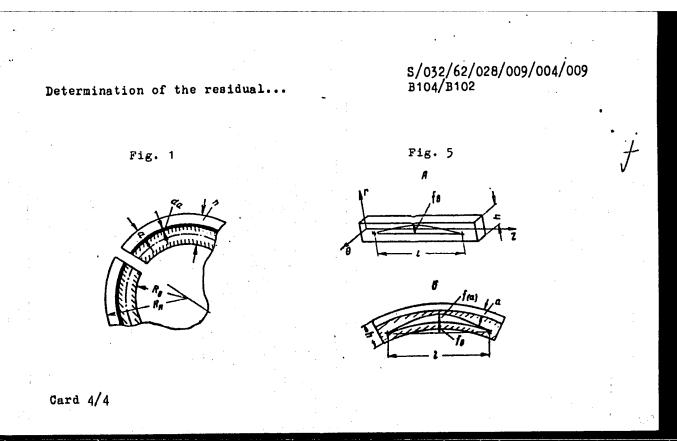
Determination of the residual...

S/032/62/028/009/004/009 B104/B102

$$U_{0}(a) = \pm \left\{ 2 \frac{E_{\delta p}}{(1 - \mu^{2}) D_{cp}^{2}} \left(\frac{h}{2} - a \right) - \frac{1}{3} \frac{E(h - a)^{3}}{(1 - \mu^{3}) D^{3}(a)} \frac{d \delta}{da} + \frac{2E}{2(1 - \mu^{3})} \left(\frac{a^{2} - 3a + \xi}{2(1 - \mu^{3})} \frac{d \delta}{da} \right) \right\}, (35)$$

where $\delta_{\ p}$ is the increase of the tube diameter after the strip is cut out. There are 6 figures.

Card 3/4



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\$/032/62/028/012/011/023

B104/B186

10.8100

AUTHOR:

Birger, I. A.

TITLE:

Determination of residual stresses in hollow and in massive

cylinders

PERIODICAL:

Zavodskaya laboratoriya, v. 28, no. 12, 1962, 1482-1484

TEXT: Assuming the radial and tangential residual stresses in a thin disk, cut from a cylinder, to be the same as those in the cylinder; assuming also that the axial stress across the thickness is constant and that the residual stresses have axial symmetry, the theory of elasticity is used to arrive at the formulas

 $\mathbf{e}_{\theta}(r) = \mathbf{e}_{\theta}^{*}(r) + \mu \mathbf{e}_{g}(r) - \frac{\mu}{r^{0}} \int_{R_{0}}^{r} r \mathbf{e}_{g} dr; \qquad (10)$ $\mathbf{e}_{r}(r) = \mathbf{e}_{r}^{*}(r) + \frac{\mu}{r^{0}} \int_{R_{0}}^{r} r \mathbf{e}_{g} dr. \qquad (11)$

 $\sigma_{\Omega}^{*}(\mathbf{r})$ and $\sigma_{\mathbf{r}}^{*}(\mathbf{r})$ can be determined for the radial and tangential stresses.

Card 1/3

Determination of residual stresses...

S/032/62/028/012/011/023 B104/B186

by known methods as described in a previous paper (I. A. Birger, Zavodskaya laboratoriya, 28, 7, 859 (1962)). Here a method of determining the axial residual stresses in a cylinder is described. Two symmetrical grooves are cut from a cylinder (Fig. 3) and the strain $t_{02}(r)$ on the outer surface is then determined. Neglecting the edge effects on the bottom of the grooves and the radial strain the axial stress is

$$\sigma_{x}(r) = -\frac{E}{2\mu (1+\mu)r} \frac{dF(r)}{dr}, \qquad (15),$$

X

where $F(r) = \frac{1}{100}(r)f(r)$ is a known function which is approximated parabolically. Using the formulas (10), (11) and (15) one can thus calculate the residual stresses in a cylinder from the strain that arises when thin disks and grooves are cut out. There are 3 figures.

Card 2/3

BIRGER, I.A.; KOLOSOV, M.A., insh., retsenzent; BYSTRITSKAYA, V.V., inzh., red.; DEMKINA, N.F., tekhn. red.

[Residual stresses] Ostatochnye napriazheniia. Moskva, Mashgiz, 1963. 231 p. (MIRA 16:11) (Stains and stresses)

BIRGER, I.A. (Moskva)

Method of additional deformations in problems of the plasticity theory. Izv.AN SSSR.Otd.tekh.nauk.Mekh.i mashinostr. no.1:47-56 Ja-F 163. (MIRA 16:2)

(Plasticity)
(Deformations (Mechanics))

AML008928

BOOK EXPLOITATION

s/

Birger, I. A.

Residual Stresses (Ostatochnywye napryazheniya) Moscow, Mashgiz, 1963, 231 p. illus., biblio., 4,000 copies printed.

TOPIC TAGS: residual stress, rod, plate, thinwalled tube, turbine disc, cylinder, x ray determination, turbine blade, steel 18KhNVA, steel 18KhNMA, steel KhVG, alloy EI 437A, alloy EI 437

PURPOSE AND COVERAGE: This book discusses the formation of residual stresses in metals and their influence on strength in static and cyclic loading. Methods of determining and analyzing residual stresses in rods, plates, tubes, discs, cylinders, and the surface layers of parts of complex configuration are described. The book is intended for engineers, designers, and researchers working in the machine building specialties.

TABLE OF CONTENTS:

Introduction - - 3 Ch. I. Formation of residual stresses - - 5

Cardel /2

BIRGER, I. A. (Moscow)

"The methods of elastic solutions in the problems of the theory of plasticity and creep"

report presented at the 2nd All-Union Congress on Theoretical and Applied Mechanics, Moscow, 29 Jan - 5 Feb 1964.

ACCESSION NR: AP4018444

8/0179/64/000/001/0193/0198

AUTHOR: Birger, I. A. (Moscow)

TITLE: Theory of plastic flow with nonisothermal loading

SOURCE: AN SSSR. Izv. Otd. tekh. nauk. Mekhanika i mashinostroyeniye, no. 1, 1954, 193-196

TOPIC TAGS: nonisothermal loading, thermal deformation, elasticity, pliability, deformation, plastic deformation, plastic flow, elastic deformation, strain, stress

ABSTRACT: The law of plastic deformations with non-isothermal loading was studied by Prager (See Prager, V., Neizothermicheskoye deformirovaniye, Sb. "Mekhanika", No. 5 (57), IL, 1959), but practical use of this work is difficult. The present article is a generalization of the theory of plastic flow in the case of non-isothermal loading. Deformation curves are given. Orig. art. has: 6 figures, 18 formulas.

ASSOCIATION: none

SURMITTED: 14Mar63

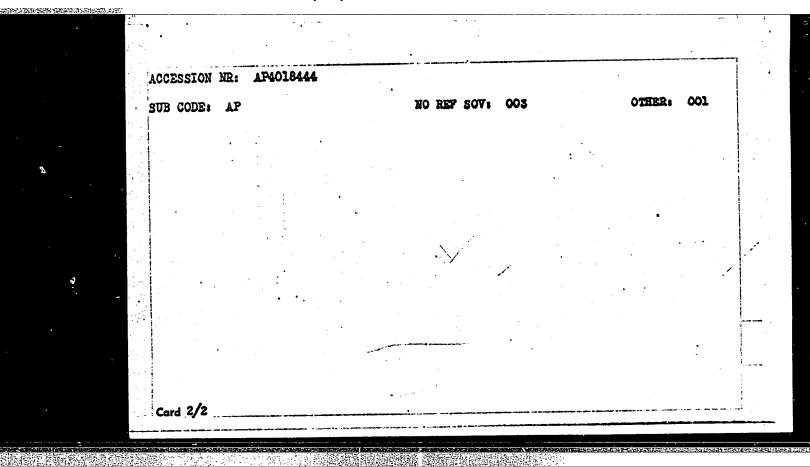
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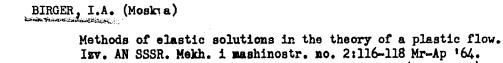
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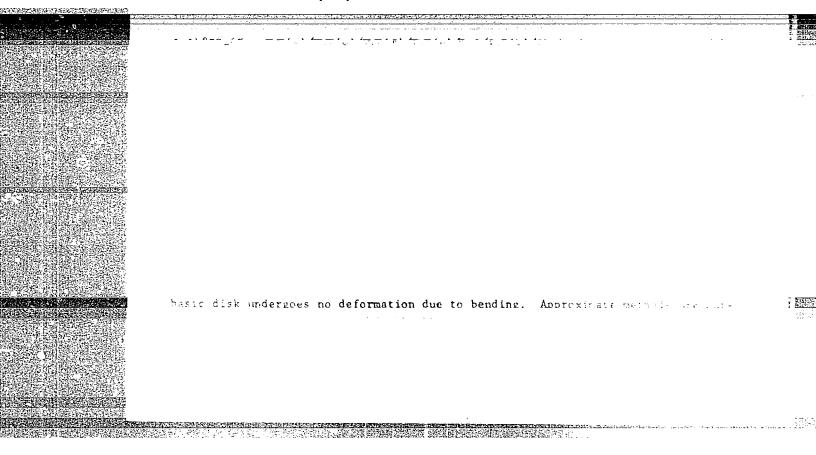
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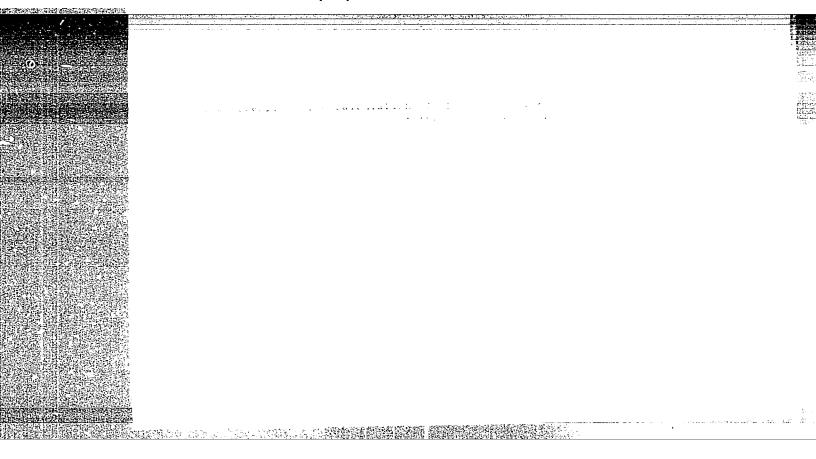
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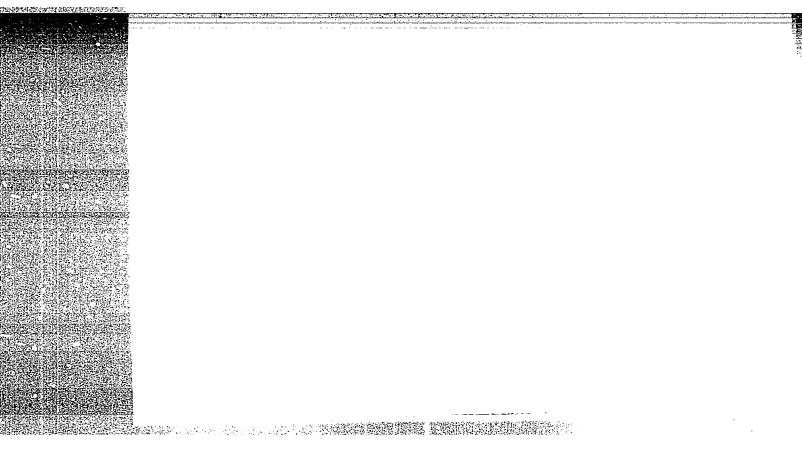




(MIRA 17:5)

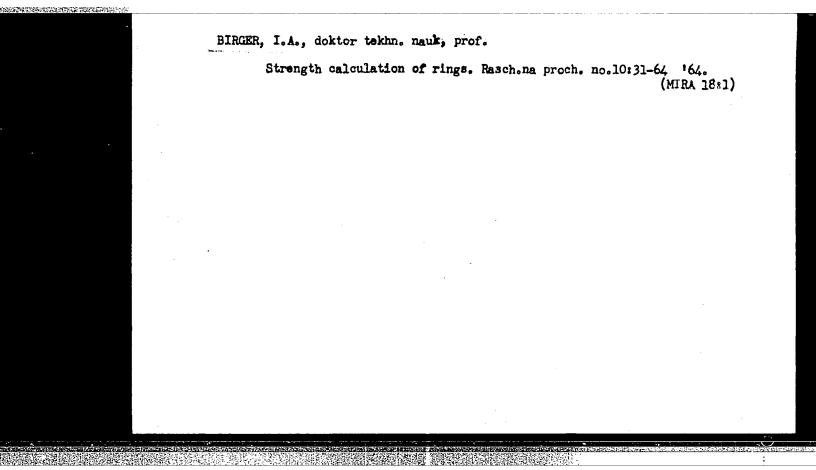


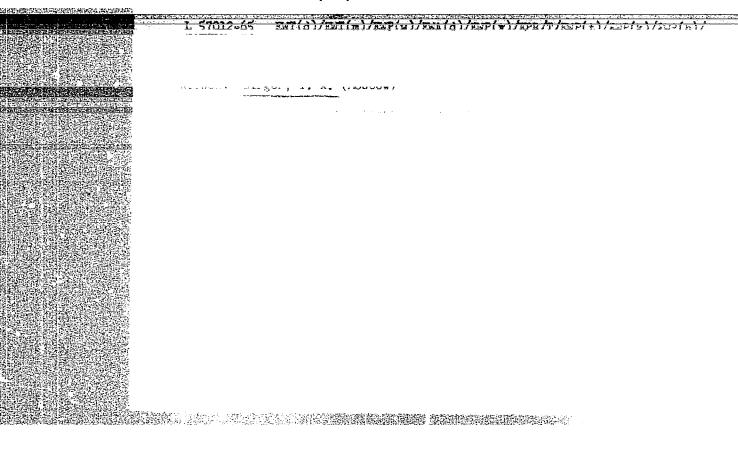




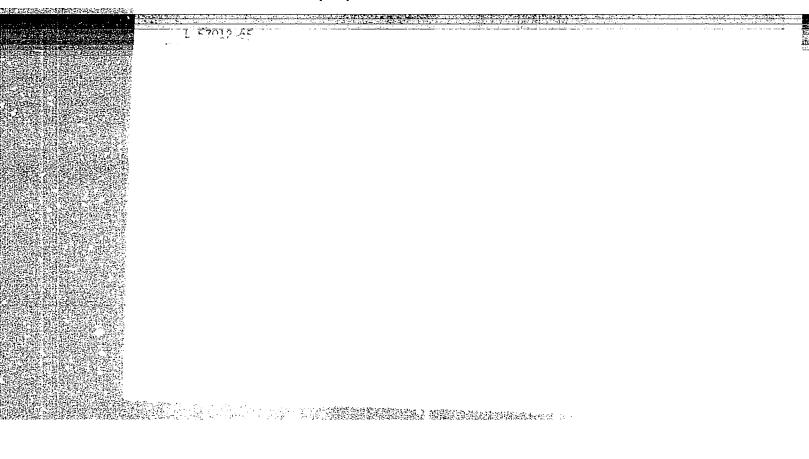
BIRGER, I.A., doktor tekhn. nauk, prof.

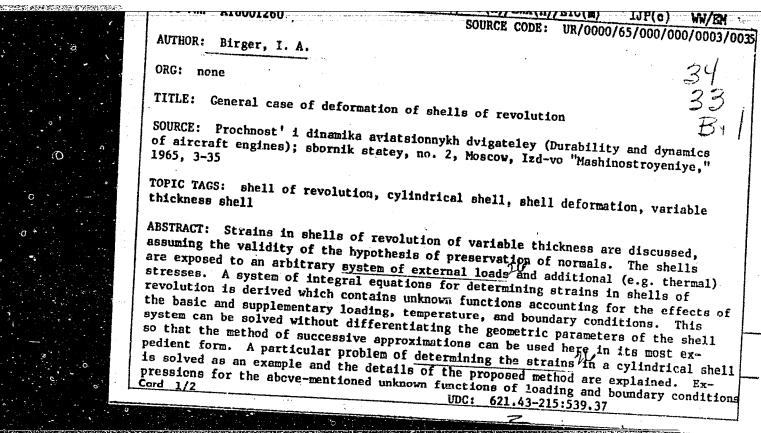
Using Bayes' formula in problems of technical diagnostics. Vest.
mashinostr. 44 no.10:24-25 0 '64. (MIRA 17:11)

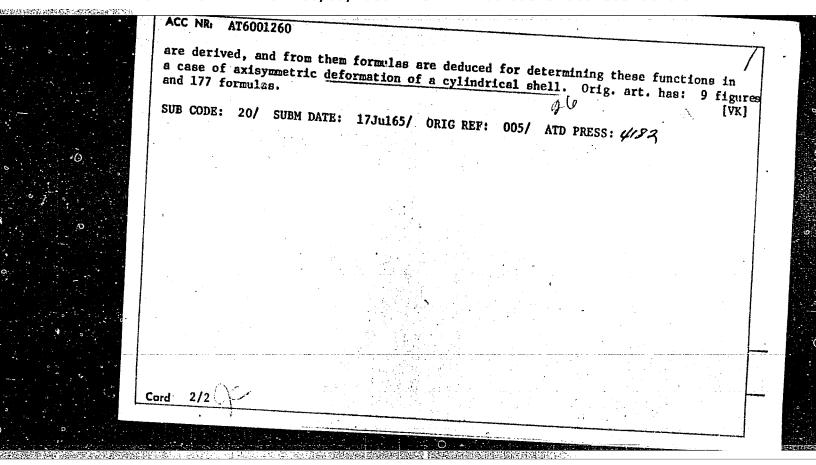










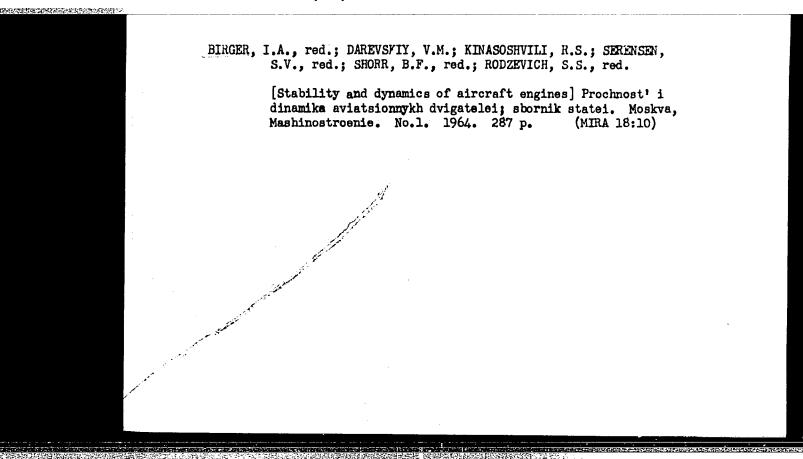


BIRGER, I.A.

A general case of the deformation of shells of revolution.

Proch. i din. av. dvig. no.2:3-35 '65.

(MIPA 18:12)



BUKIN, Mikhail Andreyevich; BIRGER, Izrail' Semenovich; MEDVEDEV, S.R., zasl. deyatel' nauki i tekhniki RSFSR, Laureat Gosudarstvennoy premii, prof., red.; BAKUN, A., red.; CHEPELEVA, O., tekhn. red.

[Largest in the world; history of the construction of the Volga Hydroelectric Power Station (22d Congress of the CPSU)] Krupneishaia v Mire; k istorii sozdaniia Volshskoi GES imeni XXII sⁿezda KPSS. Moskva, Sotsekgis, 1962. 225 p. (MIRA 16:4) (Volga Hydroelectric Power Station (22d Concress of the CPSU))—Design and construction)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"



Effect of reflections on the power-output base calibration of standard-signal oscillators used for superhigh frequency bands. Ism.tekh. no.5:40-43 \$50 '56. (MLRA 10:2) (Oscillators, Electron-tube) (Calibration)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

	BIRGER,	L.A.	:-						
		Evaluating the nonlinearity of diode mixers. Ism. tekh. no.6:77-80 H-D '57. (Blectronic instruments)							
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					•				
•						•			

05/44

S/115/60/000/011/011/013 B019/B058

9.1300 (2703, \$803,1006)

AUTHOR:

Birger, L. A.

TITLE:

Nonlinearity of a Cutoff Attenuator Caused Through Load

Reactance

PERIODICAL:

Izmeritel'naya tekhnika, 1960, No. 11, pp. 49 - 51

TEXT: In the introduction it is stated that the load reactance has a great influence on the nonlinearity of the attenuation of a cutoff attenuator. The calculations mentioned here are based on an equivalent circuit, representing a series connection of the voltage source and the impedances of the attenuator. A formula is derived for the nonlinearity of the attenuator:

or the attenuator: $\Delta = 4.34 \left(\frac{1}{1+x^2} e^{-0.1A_0} + \frac{2x}{\sqrt{1+x^2}} 10^{-0.05A_0} \right)$ (14)

where $x = \frac{X/X_0}{\left|X/X_0\right|} \cdot \frac{|X|}{R}$. From this formula it can be seen that the

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Nonlinearity of a Cutoff Attenuator Caused Through Load Reactance

S/115/60/000/011/011/013 B019/B058

information on the exact parameter values is immaterial for calculating the nonlinearity. On the contrary, the initial attenuation A_0 , experimentally determined, enters the formula. Furthermore, the nonlinearity greatly depends on the ratio of the reactive and active load component. Wide-band cutoff attenuators possess a great reactive load component and the field strength decreases proportionally to the increase of initial attenuation. The nonlinearity of attenuators operating with fixed frequency may be reduced by resonance tuning of the electrode circuits. There are 3 figures and 2 Soviet references.

W

Card 2/2

S/194/61/000/006/065/077 D201/D302

AUTHOR:

Birger, L.A.

TITLE:

Errors in the superheterodyne method of attenuation

measurements

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 6, 1961, 19, abstract 6 Il09 (Tr. in-tov Kom-ta standartov, mer i izmerit. priborov pri Sov. Min. SSSR, 1960, no. 44 (104), 10-27)

The block diagram of a superheterodyne measuring amplifier is given, the main sources of errors shown and formulae derived for their evaluation. The formulae which determine the overall errors, make possible the choice of rational methods of measurements; e.g. when measuring small attenuations (up to 30-50 db), the power applied to the attenuator should be such as to produce a maximum signal at the mixer output of about 1-5 microwatts. When measuring large attenuations the power of the signal should be increased to

Card 1/2

Errors in the superheterodyne...

S/194/61/000/006/065/077 D201/D302

decrease the effect of thermal noise. As an example, the evaluation of measurement errors is given for attenuations of about 30 and 80 db. The experimental data confirm the given estimate of overall errors. Abstracter's note: Complete translation

Card 2/2

S/194/61/000/010/062/082 D271/D301

6.4311

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AUTHOR:

Birger, L.A.

TITLE:

Determination of the effective temperature of noise

radiation of non-uniformly heated loads

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 10, 1961, 12, abstract 10 I85 (Tr. In-tov Komta standartov, mer i izmerit. priborov pri Sov. Min.

SSSR, 1960, no. 48 (108), 42-47)

TEXT: Calibration of noise generators is performed by comparing spectral densities of noise radiation of the calibrated and standard generator. A comparison amplifier is used for this purpose. Its input inevitably generates some noise radiation; switching from one noise generator to the other causes a change of the circuit impedance connected to the amplifier input, the level of amplifier noise is changed an in consequence an error occurs in measuring the ratio of spectral densities. Reflections can also cause

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Card 1/2

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

Determination of the effective ...

S/194/61/000/010/062/082 D271/D301

errors similar to those occurring in the measurements of monochromatic signals. A method is presented for calculating calibration errors of noise generators caused by reflections in a real measuring system. The block diagram of the comparator and calibration ing system. The block diagram of the comparator and calibration in even which it is used are described, and a formula is derprocedure, for which it is used are described, and a formula is derprocedure, for which it is used are described, and a formula is derprocedure, for which it is used are described, and a formula is derprocedured in the reflection coefficient corresponding to a given accuracy of measurement. The numerical example which is given shows that even when an ampliture with a very low noise input is used and the noise sources are fier with a very low noise input is used and the noise sources are very accurately matched for equal values of full output impedances, the calibration error is still fairly substantial; impedance matching mentioned above can be only obtained by the use of brdige circuits. 2 figures. 4 references. Abstracter's note: Complete translation

Card 2/2

6.4311 6.9450

131839 194/61/000/010/060/082

AUTHOR:

Birger, L.A.

TITLE:

Calibration error of noise generators due to reflec-

tions

PERIODICAL:

Referativnyy zhurnal. Avtomatika i radioelektronika, no. 10, 1961, 9, abstract 10 162 (Tr. In-tov Kom-ta standartov, mer i izmerit. priborov pri Sov. Min. SSSR, 1960, no. 48 (108), 48-53)

Standard noise sources are used for calibrating gas discharge and diode noise generators in the microwave range; these sources are matched loads heated to a comparatively high temperature ("black body", thermal noise generator). Because of the large dimensions of this type of load, in practice it is not possible to achieve the necessary uniformity of temperature when ovens of technically acceptable dimensions are used. The problem, therefore, arises of computing the effective temperature of noise radiation

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31839 S/194/61/000/010/060/082 D271/D301

Calibration error ...

of a non-uniformly heated load and of calculating losses of the thermally insulating sector of waveguide. The method of solving this problem is considered; it is based on Nyquist's theorem for four-terminal networks. A formula is derived, according to which noise in the load of the line composed of quadripoles connected in cascade is the sum of noise entering the input of the line attenuated by the total propagation factor of the line, and of noises contributed by individual quadripoles. The contribution of a given quadripole is determined by its temperature and insertion losses, and by the attenuation of the line between the quadripole and the load. It is proposed applying the above formula also to a non-uniformly heated lossy waveguide line: for this purpose the line is imagined divided into elementary sections by cross-sections perpendicular to its axis and spaced by a small distance dx; the entire waveguide is now considered as a cascade connection of quadripoles each with a temperature of T(x) and power transfer coefficient exp[-27(x)dx]*1 - 27(x)dx where 7(x) is the attenuation per unit length. An example of computation is given, in which numerical

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APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

Calibration error...

31839 S/194/61/000/010/060/082 D271/D301

data correspond to a standard source for a 5 cm band which had been developed. 3 figures. 3 references. Abstracter's note:

X

Card 3/3

9,2585 alm 3001

S/108/60/015/010/005/008 B012/B060

AUTHOR:

Birger, L. A., Active Member of the Society

TITLE:

Analysis of the Stability of Circuits With Automatic Phase Control of the Klystron Frequency 25

PERIODICAL:

Radiotekhnika, 1960, Vol. 15, No. 10, pp. 41-47

TEXT: In systems serving for the automatic phase control of the klystron frequency, a feedback designated here as "amplitude" feedback may appear in addition to the normal "phase" feedback. Experiments showed that this "amplitude" feedback is often the cause of the circuit instability. This parasitic feedback is investigated here. The principal block diagrams relating to an automatic phase control of the klystron frequency are shown in a Fig. (Refs. 1,2) and described. Condition (2) is written down for the stability of a system serving for the frequency automatic phase control, and formula (10) is derived. The first term at the right side of this formula denotes the normal functioning of the system. The second term denotes the parasitic amplitude feedback. The characteristic in this term is the absence of multiplier (ratio of the reference signal amplitude to Card 1/3

Analysis of the Stability of Circuits With Automatic Phase Control of the Klystron Frequency S/108/60/015/010/005/008 B012/B060

the klystron signal amplitude). This is indicative of the fact that there can be an amplitude feedback and hence the possibility of a self-excitation also in the case of a switched-off reference signal. Condition (12) is then derived for stability, which determines the admissible asymmetry in the balanced mixer for the signal from the klystron at a given intensity of the reference signal and at a given holding band (polosa uderzhaniya). The fact is pointed out that the present work does not consider stability in the simultaneous action of phase and amplitude feedback. Formula (12) was derived for the block diagram of Fig. a). Formulas (18) and (19) were derived in the same way for the block diagram of Fig. b). The following conclusions were reached: (1) The stability of a circuit constructed according to Fig. a) and involving the use of a reference signal of low intensity (o 1) can be ensured only by rendering the balanced highfrequency mixer very carefully symmetrical (see formula (12)). This fact is a major drawback of the circuit. To is the ratio of reference voltage to superhigh voltage. (2) For stabilizing the circuit for the automatic phase control with a frequency conversion (Fig. b)), a sufficient suppression of the intermediate frequency signals in the low-frequency filter

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Analysis of the Stability of Circuits With Automatic Phase Control of the Klystron Frequency S/108/60/015/010/005/008 B012/B060

must be ensured (see formula (17)). If the reference signal is large enough, the phase detector need not be exactly symmetrical. Experiments showed that the circuit stability can be ensured also when making use of an unbalanced detector. There are 1 figure and 2 references: 1 Soviet.

SUBMITTED: April 9, 1959

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Card 3/3

CIA-RDP86-00513R000205320015-3

6.4800 6.4310 6.9416 6.4311

20527

S/115/61/000/001/005/007 B128/B201

AUTHORS:

Birger, L. A., Shvetsov, P. N., Sokov, I. A.

TITLE:

Standard devices for the calibration of noise generators in the super-high frequency range

PERIODICAL: Izmeritel'naya tekhnika, no. 1, 1961, 37-40

TEXT: The authors describe a device for testing noise generators in the frequency range of from 1000-10,000 megacycles. A modulation method is employed for amplifying the weak signal. The block diagram of the device is shown in Fig. 1: 1) is the noise generator to be tested; 2) matching transformer; 3) standard noise generator; 4) device for keeping the temperatures constant; 5) tuned load (to room temperature); 7), 8), 9) waveguide connecting links; 10) signal generator; 11) waveguide branching; 12) matching transformer; eleminating parasitic noise; 16) high-frequency amplifier; 17) waveguide connecting link; 18) image frequency filter; 19) mixer; 20) heterodyne; modulated signal; 24) phase modulator; 25) indicating instrument; 26) video Card 1/3

Standard devices for ...

S/115/61/000/001/005/007 B128/B201

amplifier; 27) cathode-ray oscilloscope; 28) calibration line; 29) i.f. noise source (for compensating the i.f. noise); 30) electron modulator; 31) temperature pick-up for keeping the temperature of the standard generator constant; 32) stabilized (400 cycles) power supply unit. The noise source was tested by a comparison of the radiation temperature of the source with that of the standard generator. The measurements were made as follows: 1) tuning of the parts mentioned in 1, 2, and 5 according to amplitude and phase by means of matching transformers; 2) determination of the room temperature (T_z) by means of load (5); the room temperature usually differs from the normal temperature $(T_o = 293^{\circ}\text{K})$; 3) the standard noise generator with an effective radiation temperature is connected to the input; 4) compensation of i.f. noise by means of i.f. noise generator and connected calibration line; 5) determination of the attenuation factor

A = 10 $1 \frac{T_{RG} - T_{Z}}{T_{O} - T_{Z}}$ [db], where T_{RG} is the effective radiation temperature of the noise source to be tested. The final evaluation of the noise generator is made on the basis of equation $T_{C} - T_{C}$

Card 2/3

 $A_{RG} = A + A_e + 4.34 \cdot \frac{T_z - T_o}{T_{RG} - T_o}$ [d]

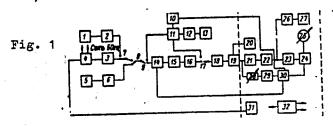
Standard devices for ...

S/115/61/000/001/005/007 B128/B201

In this equation, the last summand which is to be multiplied by the temperature-dependent parameter k, is to be neglected unless the noise source to be tested is a radiator with very low temperatures. Expression A is obtained from

 $A_e = 10 l_e \frac{T_e - T_z}{T_c}$. The error in measurement caused by the

standard noise generator $(\pm 0.08 \text{ db})$ and the measuring method $(\pm 0.14 \text{ db})$ can be reduced by repeated measurements. After the fifth measurement, it is smaller than $\pm 0.2 \text{ db}$. The authors also describe the design of the standard generator in waveguide (2600-10,000 megacycles) or coaxial construction (1000-2600 megacycles).



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Card 3/3

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

30297 S/109/61/006/011/012/021 D201/D304

9,4330

AUTHOR &

Birger, L.A.

TITLES

Bandwidth and noise factor of a tunnel diode

resonance amplifier

PERIODICAL:

Radiotekhnika i elektronika, v. 6, no. 11, 1661,

1894 - 1899

TEXT: The approximate formulae for the bandwidth $2\Delta f$ and for the noise factor F of tunnel diode resonance amplifiers given in literature, although correctly describing their fundamental properties, do not give an accurate enough assessment on the range of their applicability and are not adequate enough from the view point of a detailed design. The present article gives the results of calculations of more exact expressions for the basic resonant amplifier properties. The calculation was carried out using the generally appeted equivalent cct of a tunnel diode. Thus R_d - negative resistance in the diode; C_d - p-n junction capacitance; L_d lead incard 1/7

Bandwidth and noise factor of ...

S/109/61/006/011/012/021 D201/D304

ductance; the generator I, represents the shot noise in p-n junction; I₂ - thermal noise in r_d. The bandwidth is evaluated by calculating the gain from the equivalent cct of resonance amplifier as wen in Fig. 3. In this figure the tunnel diode parameters are those of a parallel transformation of the normal diode equivalent cct; g_L load conductance; g_g - conductance of the signal source I_g; large reactive conductance of the resonant circuit connected to the diode such that at resonance

$$b_{\text{deg}} + b_{\text{L}} = 0 \text{ if } \omega = \omega_{\text{o}}$$

 g_r — are the losses in the resonant cct. It may be defined by the ratio η of the "loaded" to "unloaded" Q of the resonant circuit

$$M = \frac{g_r}{g_g + g_L + g_r}.$$

Under these assumptions the gain defined as the ratio of the square Card 2/7

Bandwidth and noise factor of ...

S/109/61/006/011/012/021 D201/D304

root of power P_L to the maximum power of the source $P_s = I_s^2/4g_g$, is given by

$$K_{o} = \frac{2\sqrt{g_{g}g_{L}}}{g_{g} + g_{L}g_{r} + g_{deg}} = \frac{2\sqrt{s}}{\frac{1+s}{1-\gamma} - \frac{1}{R_{d}g_{g}}\frac{u(\theta)}{w(\theta)}}$$
(21)

where

$$3 = \frac{g_{L}}{g_{g}} \tag{22}$$

and u(0) is given by

$$u(\theta) = 1 - \xi - \xi \theta^2;$$
 (7)

$$w(\theta) = \theta^{2}((\xi - \frac{1}{\theta_{d}^{2}})^{2} + (1 - \xi - \frac{\theta^{2}}{\theta_{d}^{2}});$$
 (9)

in which
$$\theta = \omega \tau_d = \omega R_d C_d$$
; $\xi = \frac{r_d}{R_d}$; $\theta_d = \omega_d \tau_d$; $\omega_d = \frac{1}{\sqrt{L_d C_d}}$. By ex-

Bandwidth and noise factor of ...

s/109/61/006/011/012/021 D201/D304

pressing the loaded Q in terms of actual conductances and of resonant frequency, the bandwidth is derived as the exact

$$2\Delta j = \frac{1-\xi}{2\pi\zeta_{0}} \frac{2}{V\bar{s} + V\bar{1}/s} \frac{2}{1+p} \frac{1}{1-\eta - \frac{2}{K_{0}(V\bar{s} + V\bar{1}/s)}} \Pi(\theta), \qquad (25)$$

where

$$\Pi(0) = \frac{1 - \left(\frac{0}{0_{\mu\mu}}\right)^{2}_{e_{\mu\nu}}}{r(0)\left[1 - \frac{2}{1+p}\psi(0)\right]};$$
(26)

$$\psi(0) = \frac{\frac{\theta w'(0)}{2w(0)} - \frac{\theta v'(0)}{2v(0)}}{\frac{1}{1 - \frac{1}{\theta_{x}^{2}} \frac{\theta^{2}}{d}} - \frac{\theta^{2}}{\theta_{x}^{2}} \frac{1}{d}} + \frac{\theta^{2} \left(\xi - \frac{1}{\theta_{x}^{2}}\right)^{2} - 2\frac{\theta^{2}}{\theta_{x}^{2}}\left(1 - \xi - \frac{\theta^{2}}{\theta_{x}^{2}}\right)}{\theta^{2} \left(\xi - \frac{1}{\theta_{x}^{2}}\right)^{2} + \left(1 - \xi - \frac{\theta^{2}}{\theta_{x}^{2}}\right)^{2}},$$
(27)

and

$$p = \frac{\omega_0 b_{ab}^{\prime L}(\omega_0)}{b_{ab}(\omega_0)}. \tag{28}$$

where $\theta_{\lim} = \sqrt{1-\xi}/\xi$, $v(\theta)$ is given by Card 4/7

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Bandwidth and noise factor of ...

$$v(\theta) = 1 - \frac{1}{\theta_d^2} - \frac{\theta^2}{\theta_d^2}.$$
 (8)

In practice this equation may be reduced to that of

$$2 \triangle f = \frac{1}{2\pi \tau_{d} K_{0}} \frac{2(1-\eta)}{(\sqrt{s}+\sqrt{1/s})} \frac{2}{1+p} \left[1-\left(\frac{e}{\theta_{lim}}\right)^{2}\right]$$
 (36)

which for p = s = 1, $\eta = 0$, $(\theta/\theta_{lim})^2 = 1$ reduces to the well known formula

 $2\Delta f = \frac{1}{2\pi \tau_d K_0}.$ (37)

It is also easy to derive from Fig. 3 the exact formulae for evaluating the noise factor F:

$$F = 1 + \frac{T}{T_{s}} \frac{\eta}{q - \eta} (1 + s) + \frac{T_{s-2}}{T_{s-2}} s + \frac{1 + s}{1 - \xi} \left[\frac{1}{1 - \eta} - \frac{2}{K_{0} (\sqrt{s} + \sqrt{1/s})} \right] \frac{1}{1 - \left(\frac{\theta}{\theta_{sp}}\right)^{2} \left[\frac{eI_{0}}{2kT_{0}} + \xi (1 + \theta^{2})\right]}.$$
(38)

Card 5/7

30297 S/109/61/006/011/012/021 D201/D304

Bandwidth and noise factor of ...

It may be seen that the noise factor is independent of the self-resonant frequency of the diode θ_d . Putting $K_0 > 1$ and $T = T_L = T_g$

is obtained giving the formulae for the relative temperature t_N of the amplifier noise, where I_O in milliamps and R_d in ohms. It may be seen that when approaching the cut-off frequency the relative noise temperature increases to infinity. Thus losses and t in the diode and in the circuit and the coupling to the load must be made as small as possible (s must be reduced). This again leads to a narrower bandwidth so that a compromise must be made in the design nerower the bandwidth and noise temperature. The author acknowledges the constructive criticism of V.B. Shteynshleyger. There are 3 ges the constructive criticism of V.B. Shteynshleyger. There are 3 figures and 4 references: 1 Soviet-bloc and 3 non-Soviet-bloc. The references to the English-language publications read as follows: Card 6/7

9.3273 (also 2503)

S/108/61/016/003/004/006 B116/B205

AUTHOR:

Birger, L. A., Member of the Scientific and Technical Society for Radio Engineering and Electrocommunication

TITLE:

Stability of the circuit for the automatic control of the

klystron frequency

PERIODICAL:

Radiotekhnika, v. 16, no. 3, 1961, 40-46

TEXT: The author discusses circuits with a large number of inertial links which is characteristic of automatic phase control of klystron oscillators. He establishes the conditions for the stability of these circuits for klystrons with frequency modulation and a large number of inertial links in the feedback circuit. The inertial links formed by amplifier stages are replaced by an ideal delay line. On this basis the limiting formulas are derived. It is demonstrated that the connection of an integrating correcting circuit permits a considerable extension of the hold-in range. One of the characteristic features of automatic phase control circuits is the hold-in range ΔF_{μ} which is understood to be the maximum frequency

Card 1/4

Stability of the circuit for the ...

5/108/61/016/003/004/006 3116/3205

and the conditions

$$2\pi\Delta F_{\gamma}\frac{|\alpha(i\omega_{\alpha})|}{\omega_{\alpha}}<1,$$

(25

/равнения,

$$w_0 \tau - \operatorname{arctg} \frac{\operatorname{Im} \left[a \left(i w_0\right)\right]}{\operatorname{Re} \left[a \left(i w_0\right)\right]} = \frac{\pi}{2}$$

(26)

for the frequency of an open system. ω_0 is the root of Eq. (22), $A(\omega)$ the amplitude, $\Phi(\omega)$ the phase. With $n \ge 3$, the calculations of the stable range from the exact and from the limiting formula differ by 10% at most. It is expedient to use the limiting formulas for calculating the actual circuits with limited number of inertial links. The author then studies a circuit without correction link. Using (25) and (26) the following formulas are obtained

$$\omega_{\mathcal{F}} = \sqrt{2} \tag{27}$$

$$\Delta F_{V}^{\prime} < 1/4\tau \qquad (28)$$

i.e., with a circuit without correction links no large hold-in ranges can be obtained. By using an integrating correcting circuit (Ref. 5: R. Ley. Annales de radioelectricite. XIII. No. 33, 1958) the stable hold-in range

Card 3/4

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

S/108/61/016/012/006/009 D201/D302

9,4220 (1852,1331)

Birger, L.A., Member of the Society (See Association)

TITLE:

AUTHOR:

Frequency modulation of a phase-self-locking klystron

PERIODICAL: Radiotekhnika, v. 16, no. 12, 1961, 44-48

TEXT: In the present article the author gives the design of an FM Klystron generator from the point of view of its frequency characteristic, by considering the circuit of a phase-self-locking klystron consisting of 4 main units: A phase detector PD, connected by means of a certain connecting circuit C to the reflector of the klystron generator KG, with a delay line, being actually represented by the IF amplifier producing a delay ?, connected between the klystron output and the PD input. In real circuits the connecting circuit consists of a LP filter, d.c. amplifier and a correcting network. When considering small frequency deviations only, for which the differential equations of transients may be linearized, the operator equations are formed for each of the above units, resulting in Eq. (10)

Card 1/4

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Frequency modulation of a ...

is obtained, where $\Phi(i\Omega)$ and $\Phi_{MO}(i\Omega)$ are the modulation indices of the output and MO signal respectively which correspond to the modulation frequency of . The ratio of moduli of modulation indices may be represented as Eq. (14)

 $|\Lambda (i \Omega)| = \left| \frac{\Phi (i \Omega)}{\Phi_{xx} (i \Omega)} \right| = 2 \pi \Delta F_y \frac{|f(i \Omega)|}{|1 + 2 \pi \Delta F_y f(i \Omega)|}$

which gives for the phase shift $(i\Omega)$, resulting from FM signal, $V(i\Omega) = \text{arc tg} \frac{I_{m}[\Lambda(i\Omega)]}{\text{Re}[\Lambda(i\Omega)]} \cdot \Lambda \text{ figure shows the results}$ Eq.(15)

of numerical evaluation of Eq. (26a) for a system in which, in order to widen the stable range of oscillations, an RC correcting network is used. The relative time constant of the network is $t_k = 100$, with $\theta_{y,max} = 0.25$.

The shape of Eq. (26a) characteristic depends on the ratio of 3 of the locking range, as realized in the system, to its maximum allowable value. It may be seen that the frequency characteristic of a phase-self-locking system in FM operation depends little on the time constant $t_{\mathbf{k}}$ of the

Card 3/4

S/115/62/000/001/007/007 E192/E382

6.4311

AUTHORS: Birger, L.A. abd Sokov, I.A.

TITLE: Standard thermal noise-generators

PERIODICAL: Izmeritel'naya tekhnika, no. 1, 1962, 47 - 50

TEXT: Some improved thermal noise-generators for a wave range of 3.0 to 11.5 cm are described. The construction of the generators is illustrated in Fig. 1. A waveguide 3 with an attenuator 4 is placed inside a cylindrical oven 1, provided with suitable heaters 2. The attenuator forms a matched load. When the attenuator is heated it produces noise radiation. Provided that the temperature of the attenuator is uniform and that there are no losses between it and the output flange of the waveguide, the nominal spectral density of the radiated noise is equal to kT, where k is the Boltzmann constant and T is the attenuator temperature in K. The thermocouple 5 (see Fig.1) is employed for measuring the temperature of the

(see Fig.1) is employed for measuring the temperature of the attenuator. The wave band of 3.0 to 11.5 cm is covered by 4 separate generators based on standard waveguides of 23 x 10,

Card 1/0 3

33135 S/115/62/000/001/007/007 E192/E382

Standard thermal noise-generators

temperature and the losses in the waveguide between the attenuator and output flange. The temperature, measurement and stabilization errors are due to errors of the control system of the heater and errors of the thermocouple. These errors are of the order of ± 5 and ± 3 K, respectively. Errors caused by the nonuniform temperature distribution in the attenuator are 5 - 5 K and errors caused by losses in the waveguide are 1 - 4 K. The overall error is therefore not greater than ± 8 K, which is equivalent to ± 0.06 db. There are 2 figures, 1 table and 3 references: 2 Soviet-bloc and 1 non-Soviet-bloc. The English-language references reads as follows: Ref. 3: H. Sutcliffe - Proc.Inst.Electr.Eng., Part B, 1956, v.103, no. 11.

Card 3/ 3

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

SOKHINA, A.M.; BIRGER, M.C.

Consumption of amino soids by various pathogenic microbes. Thur, mikrobiol., epid. i immun. 42 no.3:48-52 Mr 105.

(MIRA 18:6)

1. Meskevskiy institut epidemiologii i mikrobiologii.

KHAZENSON, L.B.; BIRGER, M.Q.

Using filter paper discs for determining the sensitiveness of dysenteric pathogens to antibiotics. Lab.delo 2 no.3:23-25
My-Je '56. (MLRA 9:10)
(BACTERIA, PATHOGENIC) (ANTIBIOTICS)

BIRGER, M.O.

Decarboxylases of dysentery microorganisms. Zhur. mikrobiol. epid. 1 immun. 31 no. 10:13-17 0 '60. (MIRA 13:12)

l. Iz Moskovskogo instituta epidemiologii, mikrobiologii i gigiyeny.

(SHIGELLA) (DECARBOXYLASE)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"

SOKHINA, A.M.; BIRGER, M.O.

Amino acid consumption by microbes of the family Enterobacteriaceae. Report No.1. Zhur.mikrobiol., epid. i immun. 32 no.11:82-87 N '61. (MIRA 14:11)

1. İz Moskovskogo instituta epidemiologii, mikrobiologii i gigiyeny. (ENTEROBACTERIACEAE) (AMINO ACID METABOLISM)

KRUSHINSKAYA, Ye.A.; BOCHKOVA, V.A.; BIRGER, M.O.

Medium from dried nutrient agar for determining the toxigenicity of diphtheria microbes. Lab. delo 10 no.3:172-175 '64. (MIRA 17:5)

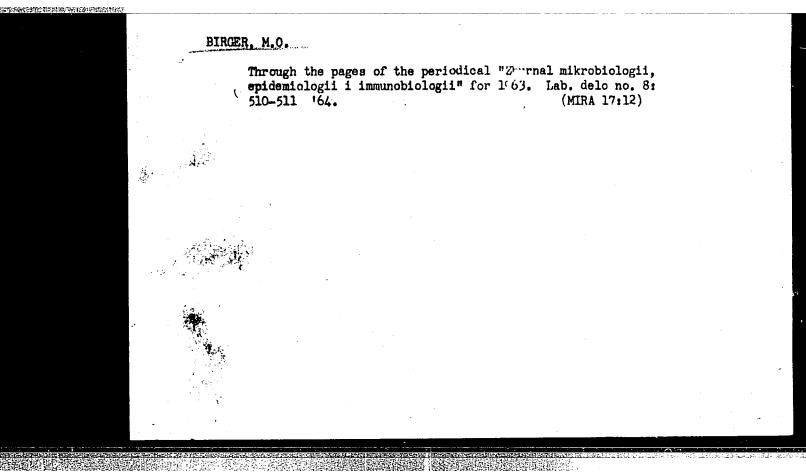
1. Moskovskiy nauchno-issledovatel'skiy institut epidemiologii i mikrobiologii.

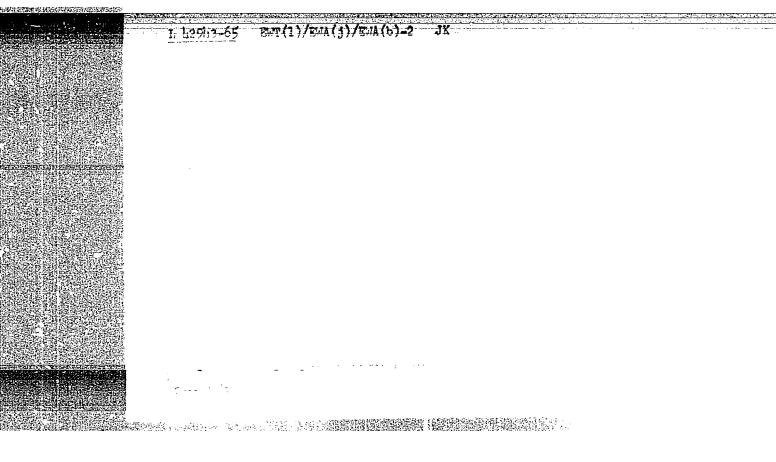
MYASNENKO, A.M.; SUMAROKOV, A.A.; BIRGER, M.O.; SHANDALOV, B.Ya.

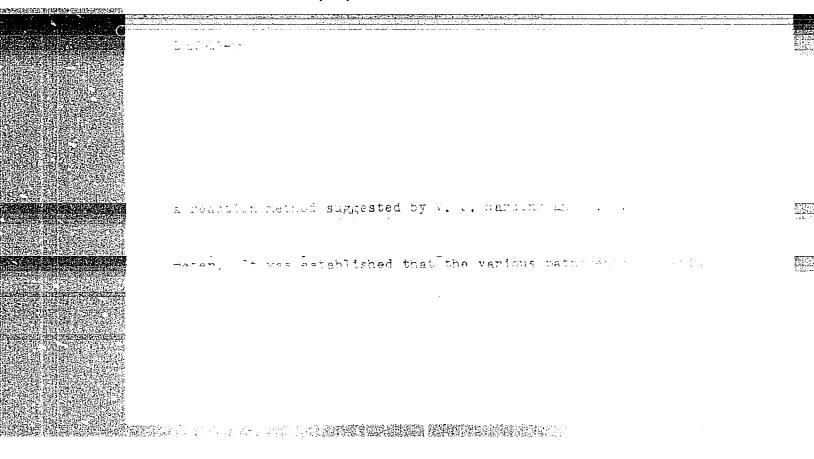
Bacteriological laboratories in the Russian Socialist Federal Soviet Republic and the organization of their work. Zdrav. Ros. Feder. 6 no.4:8-11 Ap 162. (MIRA 15:4)

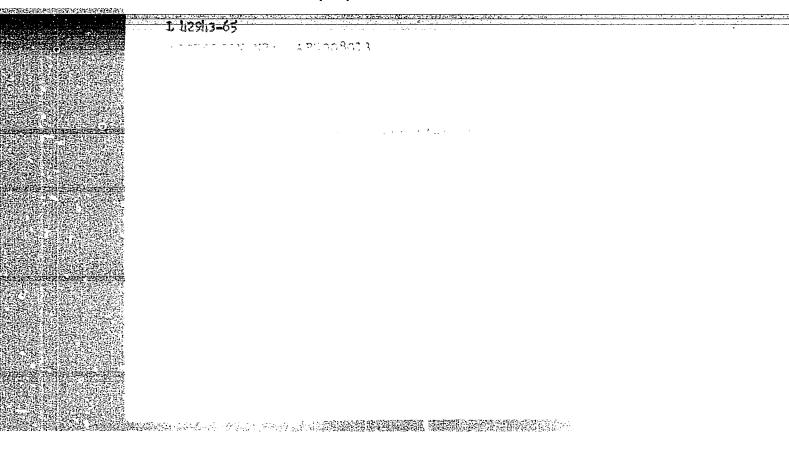
(BACTERIOLOGICAL LABORATORIES)

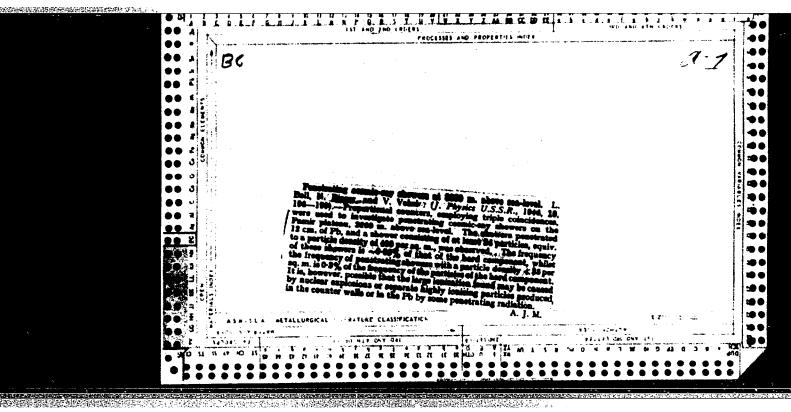
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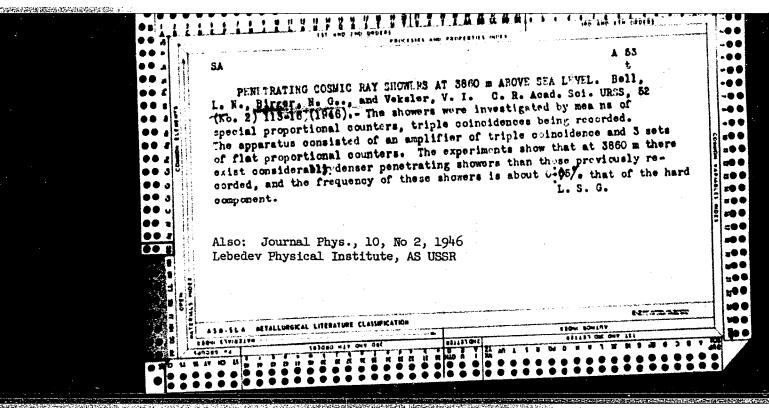






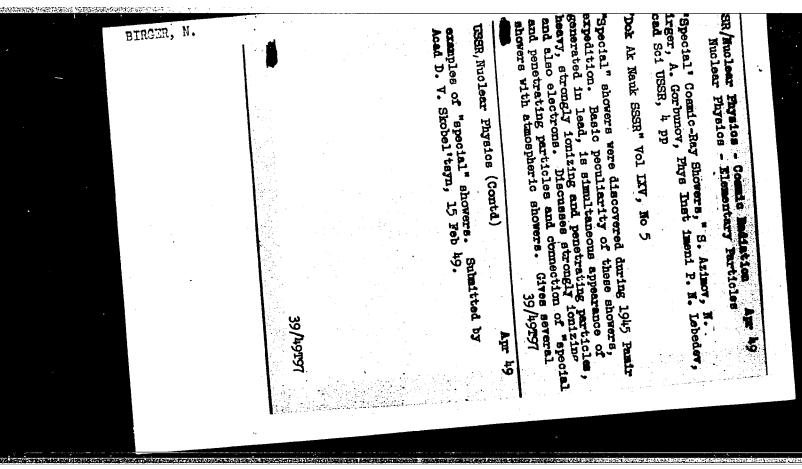






David We Us	PA 11/49T86
	**Budies of Showers Under Lead and Atmospheric Showers at Altitudes of 3,860 Meters by the Regulated Wilson Chamber Method, "M. G. Birger, Physical Lated Wilson Chamber Method, "M. G. Birger, Physical Lated Wilson Chamber Method, "M. G. Birger, Physical Instituted P. M. Lebedev, Acad Sci USER, 2 3/4 pp. **Dok Ak Mank SSER" Vol IXI, No 2 'p-145-9 Reports observations (1) of showers under lead, and cloud chamber was covered by sheet of lead 20 cm thick. Tabulates readings. In (2) following observations were made: (a) one Auger shower; (b) two showers of "explosive type (c) two showers of "li/19786 USER/Muclear Physics - Commic Redistion Jul 18 **Local" type. Submitted 15 May.46.
HERE TO BE THE RESERVE OF THE SECOND OF THE	对社会。1992年1月2日中国中国国际的国际中国国际中国国际的国际国际国际国际国际国际国际国际国际国际国际

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BIRGER, N.

PA 156T80

USSR/Nuclear Physics - Cosmic Rays Particles

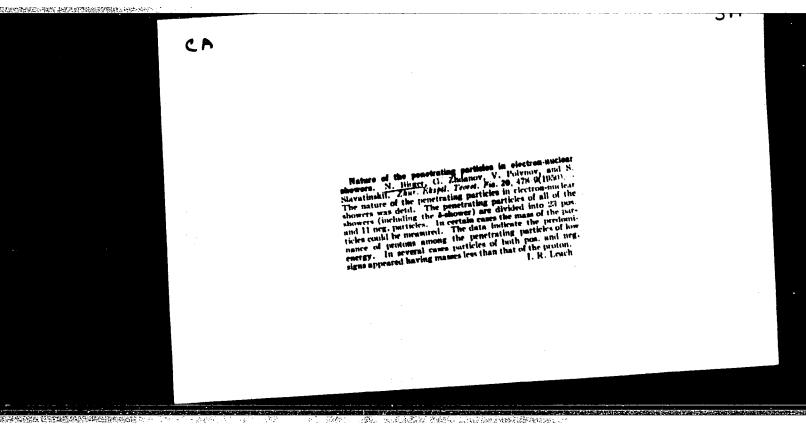
21 Apr 49

"Investigating the Nature of Particles in 'Special' Cosmic-Ray Showers," N. Birger, L. Eydus, Phys Instimeni P. N. Lebedev, Acad Sci USSR, 4 pp

"Dok Ak Nauk" Vol LXV, No 6

Discusses "special" showers studied, in 1948 in the Pamir range 3,860 meters above sea level, with aid of Wilson cloud chamber in magnetic field. Chamber was previously described by Birger ("Dok Ak Nauk USSR" Vol LXI, 1948). Tabulates number of particles as function of pulse (MeV/c). Submitted by Acad D. V. Skobeltsyn 15 Feb 49.

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BIRGER, N. G.

"Generations of Mesons in Penetrating Showers of Cosmic Rays," Uspekh. Fiz. Nauk Vol 41, No 4, 1950.

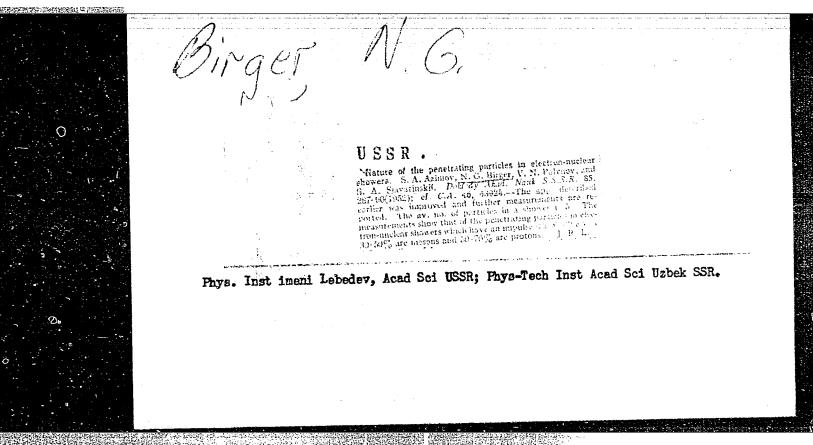
Review of current articles by N. Birger, G. Zhdanov, V. Polynov, and S. Slavatinskiy, in Zhur. Eksper i Teoret Fiz No 5, 1950.

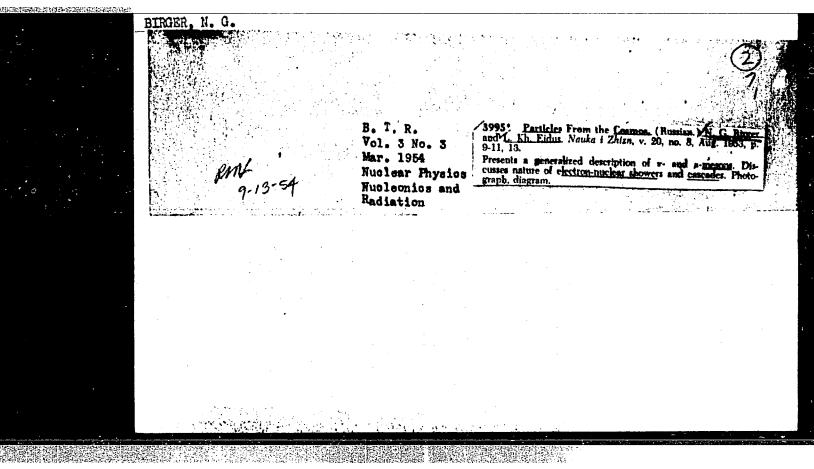
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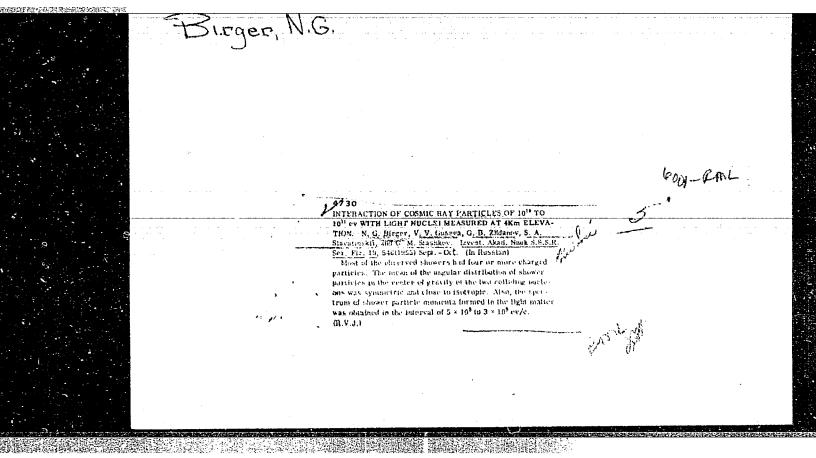
BIRGER N. G.		РА 194ТС4
	USER/ Ruclean: - Paysics (Confod) A. Lyubimov, "Dok Ak Mauk SSSR" Vol IV, 1947; and, by many others (see bibliography, p 112).	USER/Nuclear Physics Cosmic Hays "Electron Nuclear Showers and the Nuclear-Cascade Process," N. G. Birger, I. L. Rozental' "Uspekh Fiz Mauk" Vol XLV, No 1, pp 104-112 This article represents Russian response to C. F. Powell's article "Mesons" (Réports Progress in Physics, Vol XIII, 1950), translation of which appears in this same periodical. Authors make up for Powell's "forgetfulness" to quote leading works by Soviet physicists, e.g., G. Zhdanov and

"Manages of Gosmic-Ray Particles," S. Axinov, N. Bilavatinskiy, Phys Inst imeni Lebedev, Acad Sci USBR "Dok Ak Nauk SESR" Vol IXXVIII, No 3, pp 447-450 Authors' data shows that A- and 77-mesons are not predominant. Particles of mass intermediate between 7-meson and proton and with lifetime over 10-6 sec occur at 3-4 km altitudes; they do not exceed 10% of observed protons. These results differ from those of Alikhanyan and Alikhanov. Authors were assisted by savice of Acad D. V. Skobeltsyn, V. I. Veksler, 1. Psymberg, and G. T. Zatepin. App used was built with assistance of A. G. Novikov, A. A. Malinkin, V. N. Polynov, and G. I. Sergeyev. Submitted by D. Y. Skobeltsyn. 186798 E. Skobeltsyn.
21 May 51 Aximov, N. Rokurin, S. Rokurin B. Rokurin Hose Rer from those Resisted Ref 186798 Remov, Prof S. Rubmitted by D. Rokurin, Rubmitted by D. Rokurin, Rubmitted by D.

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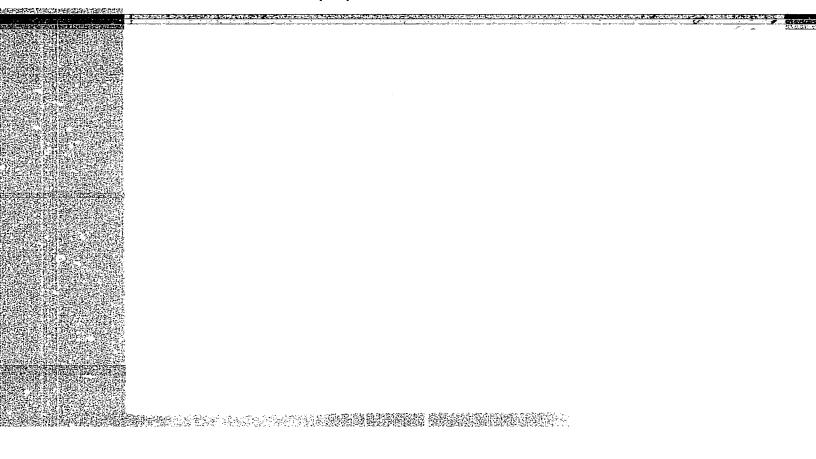




BIRGER, N.G., kandidat fisiko-matematicheskikh nauk; RAZORENOV, L.A., kandidat fisiko-matematicheskikh nauk

Mesons. Hauka i shisn' 22 no.7:21-23 Jl '55. (MIRA 8:9) (Mesons)

APPROVED FOR RELEASE: 06/08/2000 CIA-RDP86-00513R000205320015-3"



ISTRULF, IV Category : USSR/Nuclear Physics - Hlementary Particles

C-3

Abs Jour : Ref Zhur - Fizika, No 1, 1957, No 421

: Birger, M.G., Guseva, V.V., Zhdanov, G.B., Slavatinskiy, S.A., Author

Stashkov, G.M.

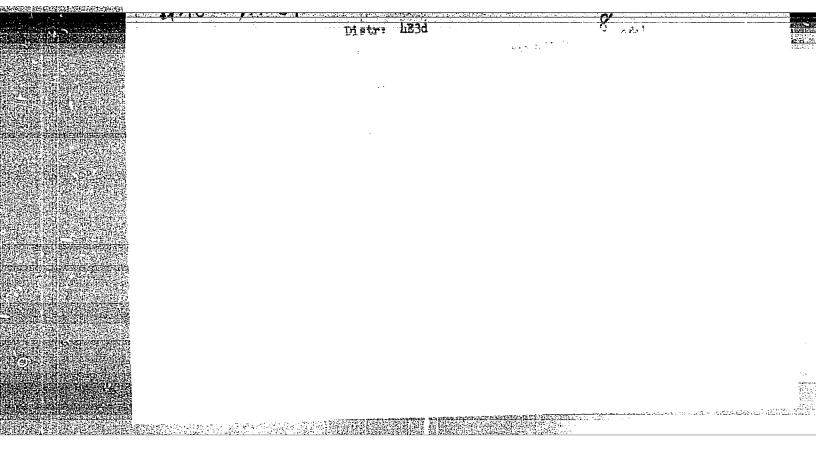
: Phys. Inst., USSR Acad. of Sciences Inst

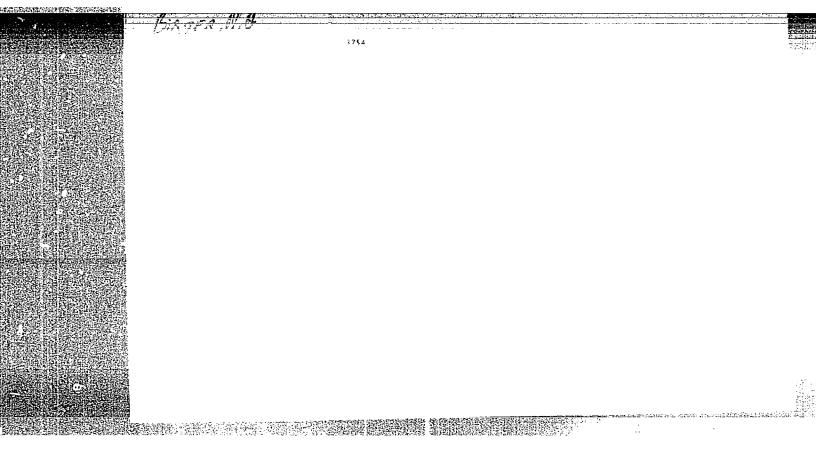
: Certain Cases of Generation of Heavy Particles by Nuclei of Be Atoms. Title

Orig Pub : Zh. eksperim. i teor. fiziki, 1956, 30, No 3, 590-591

Abstract : A Wilson chamber placed in a magnetic field and located at an altitude of 3860 meters above sea level recorded three showers, generated in Be, in which the formation and decay in flight of ξ^+ , Λ^0 , and θ^0 heavy particles. The angles (between the plane of generation of the unstable particle; and the plane of its decay are $57 \pm 10^{\circ}$, $74 \pm 10^{\circ}$, and $15 \pm 5^{\circ}$ respectively. These results can be compared with the fact that in the case of pair generation of hyperons and K-particles by π -mesons and H, the angle φ is in every case less than or equal to 40°. The difference in the results obtained is apparently due to the presence of secondary processes occurring inside the Be nucleus (scattering of hyperons or creation of hyperons by secondary particles of the shower).

: 1/1 Card





AUTHOR: BIRGER, N.G., RIGOROV, N.L.G., GUSEVA, V.V., ZDANOV, G.B. PA - 2005

SLAVATINSKIJ, S.A., STASKOV, G.M.

TITLE: Interaction between Particles of the Cosmic Radiation of the Energy

5.109-5.1010 eV and the Nuclei of Be-Atoms.

PERIODICAL: Zhurnal Eksperimental'noi i Teoret. Fiziki, 1956, Vol 31, Nr 6,

pp 971-981 (**U.S.S.R.**)

Received: 1 / 1957 Reviewed: 3 / 1957

ABSTRACT: This paper studies the production of mesons by particles of the cosmic radiation of more than 5.109 eV under conditions which resemble nucleon-nucleon collision as much as possible. For this purpose the authors arranged a WILSON chamber with a Be-plate of 9,8 g/cm² thickness in the magnetic field of an electro-magnet of the mean field strength 8500 grsted. This WILSON chamber was controlled by a system of counters. These measurements (Scientific Station PAMIR, height 3860 m) lasted a total of 950 hours and furnished about 5300 photographs. 31 photographs show electron nuclear showers with four and more particles and about 10 showers with less (2 or 3) secondary particles were observed. As the eventshetected by the measuring device amount to about 10% of all interaction acts between nucleons of > 5.109 eV and atomic nuclei, showers with few particles are likely to be formed in the case of many interaction acts in the case of the energies mentioned. In this case only the characteristics of those interaction acts are considered on the occasion of which at least four secondary particles are emitted. The corresponding data for these showers are CARD 1 / 2

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BIRGER, N.G.

PA - 1848 CARD 1 / 2 BIRGER, N.G., GUSEVA, V.V., KOTEL'NIKOV, K.A., MAKSIMENKO, V.M., SUBJECT

RJABIKOV, S.V., SLAVATINSKIJ, S.A., STAŠKOV, G.M. AUTHOR

The Analysis of the Cases of the Production of Mesons by Par-

TITLE ticles of Cosmic Radiation. II.

Žurn. eksp. i teor. fis, 31, fasc. 6, 982-986 (1956)

PERIODICAL

Issued: 1 / 1957

Three such cases are described here. For the direct measuring of the energy of the particles producing electron-nucleon showers the authors in the winter of 1955-1956 added a further WILSON chamber fitted below the gap of the electromagnet to their apparatus (described by BIRGER et al., Zurn.eksp.i teor. fis, 31, 971 (1956)). The charged particle is deflected after passage through the upper chamber by the field of the electromagnet with a field strength of about 104 Ørsted. In the lower chamber the trace of the primary particle can be followed on a beryllium plate, and from the traces of the secondary particles the point of the production of the shower in the beryllium plate is determined. From the deviation of this point from the direction of the motion of the particle before being deflected in the magnetic field it is possible to determine the momentum and the sign of the charge of the shower-producing particle. In the case under investigation p = 50 BeV/c. However, by using two WILSON chambers the "light intensity" of the device was considerably diminished. Altogether, four pictures of showers with more than four charged secondary particles were taken, from which it was possible to determine

VIL'SON, Dzh. [Wilson, J.G.], red.; BAYYER, V.N. [translator]; MAKSIMENKO, V.M. [translator]; SARYCHEVA, L.I. [translator]; BIRGER, N.G., red.; ROZENTAL', I.L., red.; NAKHIMSON, I.G., red.; KHAR'KOVSKAYA, L.M., tekhn.red.

[Physics of cosmic rays; modern achievements] Fizika kosmicheskikh luchei; sovremennye dostisheniia. Sost. gruppoi avtorov. Pod red. Dsh.Vil'sona. Moskva, Isd-vo inostr.lit-ry. Vol.3. 1958. 444 p. Translated from the English. (MIRA 13:6)

BIRGER, N.G-

CONCERNING A PECULIARITY IN THE INTERACTION OF PARTICLES WITH ENERGY

N. Birger, S. Slavatinskiy, Yu. Smorodin

Kinematic analysis is applied to photographs of the interaction of nucleons of energy $E_0 > 10^{11}$ ev with nuclei. From conservation laws it follows that the magnitude $(E_1 - P_1) + P_1$ (I $-\cos O_1$) is close to the mass of the target.

In most cases of the observed interactions summation over all registered particles yields a value on the left-hand side that is close to the mass of a pimeson. If the possibility of a less of pimeson emerging at angles close to 90° is excluded, then the pimeson should be considered as the target in the cases considered.

Report presented at the International Cosmic Ray Conference, Moscow, 6-11 July 1959

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24(5) AUTHORS:

Birger, N. G., Smorodin, Yu. A.

sov/56-36-4-30/70

TITLE:

On the Kinematics of Elementary Interactions (O kinematike

elementarnykh vzaimodeystviy)

PERIODICAL:

Zhurnal eksperimental noy i teoreticheskoy fiziki, 1959,

Vol 36, Nr 4, pp 1159-1167 (USSR)

ABSTRACT:

The investigation of the interaction between high-energy particles (>10°ev) and nucleons and nuclei meets with difficulties caused by the following two main reasons: As no complete theoretical description of the interaction processes is available, the existing experimental material cannot be analyzed according to uniform points of view; the experimental devices used today for the purpose of investigating the interaction of fast particles (cosmic radiation, accelerator) do not render a complete determination of the processes observed possible. The object of the present paper is the consideration of some kinematic methods of analyzing nuclear interactions of fast particles. This analysis furnishes individual partial process characteristics which are free from representations using the similarity method (model representations). By employing the theorems of conservation, the authors derive a

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On the Kinematics of Elementary Interactions

SOV/56-36-4-30/70

number of interaction relations; thus, an expression is given for the number k of particles contained in a given solid angle for the case in which, in the c.m.s., the nucleons fly off isotropically. Also for k_{\max} a formula is derived. The

relations obtained are finally applied to experimental data. The analysis of such interactions observed in cloud chambers and photographic emulsions in the c.m.s of the colliding particles (of tables 1 and 2) supplies angular and energy characteristics of the interactions. The results obtained by these investigations are discussed in detail. The authors thank the staff members of the Laboratoriya kosmicheskikh luchey FIAN (Laboratory for Cosmic Radiation of the Physics Institute of the AS) and of the NIMaF (Scientific Research Institute for Nuclear Physics) for discussions. There are 5 figures, 2 tables, and 13 references, 7 of which are Soviet.

ASSOCIATION:

Fizicheskiy institut im. P. N. Lebedeva Akademii nauk SSSR (Physics Institute imeni P. N. Lebedev of the Academy of Sciences, USSR)

Card 2/3

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S/058/61/000/010/018/100 A001/A101

3.2410

AUTHORS:

Birger, N.G., Slavatinskiy, S.A., Smorodin, Yu.A.

TITLE:

On one peculiarity of interaction of particles with average energy

of 200 Bev

PERIODICAL:

Referativnyy zhurnal, Fizika, no. 10, 1961, 96, abstract 10B502

("Tr. Mezhdunar, kenferentsii po kosmich, lucham, 1959, v. 1", Mos-

gow, AN SSSR, 1960, 154 - 156)

TEXT: Kinematical method of analysis is applied to investigations of interactions of particles with average energy of 200 Bev. The method makes it

possible to determine effective mass of the target nucleus.

[Abstracter's note: Complete translation]

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BIRGER, N. G., SMORODIN, YU. A.,

"On the Interactions of Mesons and Nucleons."

report submitted for the Intl. Conf. on Cosmic Rays and Earth Storm (IUPAP) Kyoto, Japan 4-15 Sept. 1961.

BIRGER. N.G.; WANG KANG-CH'ANG; WANG TS'U-TSÊNG; TING TA-TS'AO; KATYSHEV,
1U.V.; KLADNITSKAYA, Ye.N.; KOPYLOVA, D.K.; LYUBIMOV, V.B.; HGUEN
DIN TY; HIKITIN, A.V.; PODGORETSKIY, M.I.; SOLOV'YEV, M.I.

[Inelastic interaction of 6.8 Bev/s JT -mesons and nucleons]
Neuprugie vzaimodeistviia JT -mezonov s impul'som 6,8 Bev/s s
neuklonami. Dubna, Obmedinennyi in-t iadernykh issl., 1961. 30 p.
(MIRA 14:11)

(Mesons)

(Nucleons)

BIRGER, N.G.; VAN GAN-CHAN [Wang Kang-ch'ang]; VAN TSU-TSZEN [Wang TS'u-tsêng];
DIN DA-TSAO [Ting Ta-ts'ao]; KATYSHEV, Yu.V.; KLADNITSKAYA, Ye.N.;
KOPYLOVA, D.K.; LYUBIMOV, V.B.; NGUYEN DIN TY; NIKITIN, A.V.;
PODGORETSKIY, M.I.; SMORODIN, Yu.A.; SOLOV'YEV, M.I.; TRKA, Z.

Inelastic interactions of 6.8 Bev./c 7 mesons with nucleons. Zhur. eksp. i teor. fiz. 41 no.5:1461-1474 N '61. (MIRA 14:12)

1. Ob"yedinennyy institut yadernykh-issledovaniy.
(Collisions (Nuclear physics))
(Mesons) (Nucleons)

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S/056/62/043/001/049/056 B102/B104

24.6600

AUTHORS: Bayukov, Yu. D., Birger, N. G., Leksin, G. A., Suchkov, D. A.

TITLE: The nature of elastic πN and pp scattering in the region of

large transferred momenta

PERIODICAL: Zhurnal eksperimental noy i teoreticheskoy fiziki, v. 43,

no. 1(7), 1962, 339-341

TEXT: The results of experimental and theoretical papers concerning elastic πN and pp-scattering with transferred momenta >0.5 Bev/c are reviewed, discussing mainly the energy course of the differential elastic scattering cross section. Investigations of the asymptotic behavior of

the scattering amplitude point to a relation $d\sigma_{el}/dt = f(t)s^2[1(t)-1]$

where t is the square of the transferred four-momentum and s is that of the total particle energy in the c. m. s. Numerical results from several papers are used to study the |t| - dependence of l(t) at t-values of from 0.5 to 2.4 $(\text{Bev/c})^2$ and s up to 52 $(\text{Bev})^2$. It is found that l(t) drops

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